

COBALT(II) REMOVAL FROM SYNTHETIC WASTEWATER BY ADSORPTION ON SOUTH AFRICAN COAL FLY ASH

Authors:

Evans T. Musapatika¹
Maurice S. Onyango²
Ochieng Aoyi³

Affiliations:

¹School of Chemical and Metallurgical Engineering, University of the Witwatersrand, South Africa

²Department of Chemical and Metallurgical Engineering, Tshwane University of Technology, Pretoria, South Africa

³Department of Chemical Engineering, Vaal University of Technology, South Africa

Correspondence to:

Evans Musapatika

email:

uzchemist@yahoo.com

Postal address:

School of Chemical and Metallurgical Engineering, University of the Witwatersrand, Private Bag X3, Wits 2050, South Africa

Keywords:

adsorption; coal fly ash; cobalt (II); isotherm; response surface methodology; wastewater

Dates:

Received: 30 Oct. 2009

Accepted: 16 Aug. 2010

Published: 04 Oct. 2010

How to cite this article:

Musapatika ET, Onyango MS, Aoyi O. Cobalt(II) removal from synthetic wastewater by adsorption on South African coal fly ash. *S Afr J Sci.* 2010;106(9/10), Art. #167, 7 pages. DOI: 10.4102/sajs.v106i9/10.167

This article is available at:

<http://www.sajs.co.za>

© 2010. The Authors.
Licensee: OpenJournals Publishing. This work is licensed under the Creative Commons Attribution License.

ABSTRACT

Advanced wastewater-treatment techniques such as adsorption are essential in the removal of non-biodegradable toxic wastes from water. In this study, the use of South African coal fly ash, an industrial byproduct, has been investigated as a potential replacement for the current costly adsorbents used for removing heavy metals from wastewater. We utilised coal fly ash for the adsorption of cobalt(II) ions from synthetic petrochemical wastewater and characterised its performance. A two-level three-factor full-factorial design was successfully employed for experimental design and analysis of the results. The combined effects of pH, initial concentration and adsorbent dose on cobalt(II) removal were assessed using response surface methodology. Although the focus was on removal of cobalt(II), the adsorption was carried out in the presence of phenol and other heavy metal ions using the batch technique. The applicability of the Freundlich and Langmuir models to the equilibrium data was tested. Consequently, the equilibrium data was found to conform more favourably to the Freundlich isotherm than to the Langmuir isotherm; in this case, the coal fly ash had a maximum adsorption capacity of 0.401 mg/g for cobalt(II). We conclude that South African coal fly ash, as a natural, abundant and low-cost adsorbent, might be a suitable local alternative for elimination of cobalt(II) from aqueous solutions.

INTRODUCTION

The removal of recalcitrant contaminants, such as cobalt, from wastewater is essential as they pose a serious health and environmental hazard. Severe effects of acute cobalt poisoning in humans include asthmatic symptoms and damage to the heart, thyroid and liver. At elevated concentrations, cobalt may also cause genetic mutations in living cells, emphasising the need to increase awareness of the problems associated with cobalt poisoning.

Current studies related to the method of removing cobalt from wastewater have drawn broad interest and show that cobalt removal from wastewater cannot be adequately achieved using secondary adsorption methods.¹ Thus advanced wastewater-treatment methods, such as ion exchange,² precipitation,³ membrane separation⁴ and electrolysis,⁵ must be used to remove recalcitrant waste such as cobalt. However, most of these methods are costly and require high levels of expertise; consequently, these methods are not applied by many end-users. For these reasons, adsorption technology has gained a wider application due to its inherent low cost, simplicity, versatility and robustness.

The success of an adsorption process starts with choosing the appropriate adsorbent. Several adsorbents can be used to treat industrial wastewater, namely commercial activated carbon, zeolites, silica gel and activated alumina. Unfortunately, these adsorption media are relatively costly. For this reason, the use of low-cost adsorbents derived from industrial solid waste has attracted wide attention in recent years. Such waste materials currently are underutilised, which avails them for use as adsorbents.

For example, 28 million tonnes of coal fly ash, a micro-spherical particulate byproduct of high-ash content coal combustion for power generation,⁶ is produced annually in South Africa.⁷ Merely 5% of the coal fly ash is used as a construction material while the rest is stored in ash dumps that have to be rehabilitated, which results in an increase in the cost of ash handling.⁸ This coal fly ash has a high unburned carbon content and thus cannot be used as a cement additive because of the adverse effects of the carbon on the quality of concrete.⁹ Other avenues for the utilisation of the vast amounts of unused coal fly ash are therefore open for investigation. The use of coal fly ash as an alternative to costly adsorbents could benefit developing countries such as South Africa.

Several studies have shown the effectiveness of coal fly ash in the removal of heavy metals^{8,9} and organics¹⁰ from wastewater. In adsorption processes, factors such as the initial concentration of wastes, initial pH and adsorbent dose influence the process efficiency. Process efficiency may thus be optimised through adjustment of these factors.¹¹ In conventional multifactor experiments, optimisation is usually carried out by varying a single factor while keeping all the other factors fixed at a specific set of conditions – the one-factor-at-a-time (OFAT) method. However, the OFAT method is extremely time consuming and expensive because it requires a large number of experiments to be performed.¹² Furthermore, the OFAT method does not include interactive effects among the variables and does not depict the complete effects of the parameters on the process.¹¹

The limitations of traditional methods such as the OFAT method can be eliminated by optimising all the affecting parameters collectively by statistical experimental designs such as response surface methodology (RSM).¹² RSM is a collection of mathematical and statistical techniques useful for developing, improving and optimising a process and can be used to evaluate the relative significance of several affecting factors even in the presence of complex interactions. The main objective of RSM is to determine the optimum operational conditions for the system or to determine a domain that satisfies the operating specifications. The application of statistical experimental design techniques in the development of the adsorption process can result in reduced process variability and overall costs.¹³ However, RSM has not been used for the optimisation of the removal of cobalt(II) from petrochemical wastewater using coal fly ash.

The objectives of the present study were to investigate the feasibility of using South African coal fly ash for the removal of cobalt(II) from synthetic petrochemical wastewater, to model the adsorption process of cobalt(II) and to investigate the interactive effects of process parameters such as adsorbent dose, solution pH and initial concentration on the adsorption capacity of coal fly ash towards cobalt(II) ions using response surface methodology.

MATERIALS AND METHODS

Characterisation of coal fly ash

Coal fly ash collected from the Lethabo Power Station (Free State province, South Africa) was sieved to a particle size of between 53 µm and 180 µm and used without any pretreatment. X-ray diffraction (XRD) studies were carried out using an X-ray diffractometer (PANalytical, Philips PW 1710, EA Almelo, the Netherlands) with Cu Kα radiation at 40 kV and 50 mA. The X-ray pattern was recorded from 10° – 65° at a scan rate of 1.2°/min; various phases present in coal fly ash were identified. Fourier transform infrared (FTIR) spectra of the coal fly ash were recorded in the range 500 cm⁻¹ – 4000 cm⁻¹ on an FTIR (Bruker, Tensor 27 TPR, Ettlingen, Germany) system in order to explore the number and positions of the functional groups responsible for adsorption. The surface morphology of the coal fly ash was visualised using a scanning electron microscope (SEM, Jeol JSM-840, Tokyo, Japan). The specific area (*S*_{BET}) and pore structural parameters of the coal fly ash were determined from the adsorption-desorption isotherm of nitrogen at 77 K using a surface area and porosity analyser (Micromeritics, TriStar 3000, Norcross, GA, USA). The micropore volume (*V*_{mi}) and micropore specific area (*S*_{mi}) were obtained using a *t*-plot. The total pore volume (*V*_t) was obtained by converting the nitrogen adsorption amount at a relative pressure (*P*/*P*₀) of 0.98 to the liquid nitrogen volume. The mesopore volume (*V*_{me}) was calculated by subtracting *V*_{mi} from *V*_t.¹⁴

Preparation of synthetic petrochemical wastewater

The synthetic petrochemical wastewater used in this study contained phenol and the heavy metals cobalt, nickel, iron and

lead. However, in this paper, we present only the adsorption results of cobalt(II). Stock solutions (1000 mg/L) of cobalt(II), nickel(II), iron(II), lead(II) and phenol were prepared by dissolving 4.94 g of Co(NO₃)₂·6H₂O, 4.48 g of NiSO₄·6H₂O, 4.98 g of FeSO₄·7H₂O, 1.60 g of Pb(NO₃)₂ and 1.00 g of C₆H₅OH, respectively, in 1 L of distilled water. The stock solutions were diluted with distilled water to obtain the desired initial concentration according to the levels specified in Table 1. The composition of the synthetic aqueous solutions used in this study were based on those used previously¹⁵ and concentrations were within the range of the typical petrochemical wastewater described in the Pollution Prevention and Abatement Handbook,¹⁶ which specifies that the phenol concentration range is 20 mg/L – 200 mg/L and the range for heavy metals is 0.1 mg/L – 100 mg/L. The pH of the solutions was adjusted using either dilute HCl or NaOH. A maximum pH of 6, which is below the pH point of precipitation (pH_{pp}) for each of the metal ions, was chosen to prevent possible metal hydroxide precipitation.¹⁷ All the pH measurements were carried out using a pH meter (LabX Direct-SevenMulti, Mettler Toledo, Columbus, OH, USA) and all the chemicals used were of analytical grade and supplied by Merck Chemicals (Johannesburg, South Africa).

Experimental design and optimisation of parameters

The adsorbent dose, pH and initial concentration were chosen as independent variables and the adsorption capacity (*q*_e) as the dependent output response variable. A two-level three-factor full-factorial design with four centre points leading to 12 experimental runs was performed (Table 2). The centre point replicates were chosen to verify any change in the estimation procedure as a measure of precision property. For statistical calculations, the variable *X*₁ was coded as *x*₁ according to the following relationship:

$$x_i = \frac{X_i - X_0}{\Delta X} \tag{Eqn 1}$$

where *x*₁ is the independent variable coded value, *X*₁ is the independent variable real value, *X*₀ is the independent variable real value on the centre point and Δ*X* is the step change value.¹² Table 1 gives the range and the levels of the variables (i.e. low and high) investigated in this study.

The quadratic model for predicting the adsorption capacity for cobalt(II) was expressed according to the following equation:

$$y = \beta_0 + \beta_1x_1 + \beta_2x_2 + \beta_3x_3 + \beta_{11}x_1^2 + \beta_{22}x_2^2 + \beta_{33}x_3^2 + \beta_{12}x_1x_2 + \beta_{13}x_1x_3 + \beta_{23}x_2x_3 \tag{Eqn 2}$$

where *y* is the response predicted by the model and *x*₁, *x*₂ and *x*₃ are the coded forms of dose, pH and initial concentration, respectively. The term β₀ is the offset term, β₁, β₂ and β₃ are linear terms, β₁₁, β₂₂ and β₃₃ are the quadratic terms and β₁₂, β₁₃ and β₂₃ are the interaction terms. An analysis of variance (ANOVA) was performed to establish statistical significance for the quadratic model. Design Expert Version 6.0.6 (Stat-Ease Inc. in Minneapolis, USA) and Matlab Version 7.0.1 (MathWorks in Natick, Massachusetts) were used for regression and graphical analyses of the data obtained. The statistical significance of the regression coefficients was determined by the Student's *t*-test and *p* < 0.05 was considered significant.

Experimental procedure

The adsorption of cobalt(II) ions from the synthetic petrochemical wastewater was performed in a static mode (batch adsorption). A 100-mL wastewater solution of known initial concentration was contacted with a desired mass of coal fly ash in 250-mL Erlenmeyer flasks. Blank solutions (i.e. solutions without the adsorbent) were also included to correct for any adsorption by the flasks; all the flasks were covered with parafilm. The mixture was shaken at 250 rpm in an incubator with a shaking

TABLE 1
The experimental range and levels of the independent variables affecting adsorption capacity

| Factor | Symbols | | Range and levels | | |
|--------------------------------------|-----------------------|-----------------------|------------------|-----|-----|
| | Actual | Coded | -1 | 0 | 1 |
| Dose (g/L) | <i>X</i> ₁ | <i>x</i> ₁ | 20 | 40 | 60 |
| pH | <i>X</i> ₂ | <i>x</i> ₂ | 2 | 4 | 6 |
| Concentration of heavy metals (mg/L) | <i>X</i> ₃ | <i>x</i> ₃ | 25 | 50 | 75 |
| Concentration of phenol (mg/L) | <i>X</i> ₃ | <i>x</i> ₃ | 55 | 110 | 165 |

TABLE 2
The two-level three-factor full-factorial design with four centre points for the analysis of the adsorption capacity of coal fly ash for cobalt(II)

| Standard order | Coded variables values | | | Adsorption capacity, <i>q</i> _e (mg/g) | |
|----------------|------------------------|-----------------------|-----------------------|---|-----------|
| | <i>x</i> ₁ | <i>x</i> ₂ | <i>x</i> ₃ | Observed | Predicted |
| 1 | -1 | -1 | -1 | 0.023 | 0.038 |
| 2 | 1 | -1 | -1 | 0.388 | 0.373 |
| 3 | -1 | 1 | -1 | 1.083 | 1.068 |
| 4 | 1 | 1 | -1 | 0.361 | 0.376 |
| 5 | -1 | -1 | 1 | 0.06 | 0.045 |
| 6 | 1 | -1 | 1 | 1.01 | 1.025 |
| 7 | -1 | 1 | 1 | 1.118 | 1.133 |
| 8 | 1 | 1 | 1 | 1.102 | 1.087 |
| 9 | 0 | 0 | 0 | 1.085 | 1.084 |
| 10 | 0 | 0 | 0 | 1.084 | 1.084 |
| 11 | 0 | 0 | 0 | 1.085 | 1.084 |
| 12 | 0 | 0 | 0 | 1.083 | 1.084 |

*x*₁, adsorbent dose
*x*₂, pH of solution
*x*₃, initial concentration of adsorbate

platform (FSIM-SPO16, Labcon, Johannesburg, South Africa) at 25 °C for a predetermined contact time of 4 h. The supernatant was then separated by filtration. The initial and final cobalt(II) concentrations were determined using an atomic absorption spectrometer (SpectrAA 55B, Varian, Victoria, Australia) and the adsorption capacity (q_e) was calculated as:

$$q_e = \frac{(C_o - C_e)V}{m} \quad [\text{Eqn 3}]$$

where C_o and C_e are the initial and equilibrium adsorbate concentrations in solution (mg/L), respectively, V is a known volume of synthetic wastewater (L), and m is a known mass of dry coal fly ash (g).

To optimise the design of an adsorption system for the removal of adsorbate, it is important to obtain the equilibrium adsorption data. Thus the equilibrium adsorption isotherm data was generated by contacting a fixed amount of coal fly ash with 100 mL of synthetic petrochemical wastewater, in which the concentration of metal ions and phenol ranged from 20 mg/L to 90 mg/L, at a pH of 4.0 in 250-mL Erlenmeyer flasks. Coal fly ash was separated from the solution after 4 h and the residual cobalt(II) ion concentration in the solution was measured.

RESULTS AND DISCUSSION

Characterisation of coal fly ash

Adsorption is a surface phenomenon and the rate and extent of adsorption are functions of the specific surface area of the adsorbent used, i.e. the portion of the total surface area that is available for adsorption. In fact, the amount of adsorption per unit weight of an adsorbent depends on its composition, texture and porosity.¹⁸ It is apparent from Figure 1 that the crystalline phases (represented by the sharp peaks) present in the raw coal fly ash are quartz (SiO_2), mullite ($\text{Al}_6\text{Si}_2\text{O}_{13}$) and lower concentrations of haematite (Fe_2O_3) and calcium oxide (CaO) or lime. The coal fly ash is therefore alkaline and can neutralise wastewater and adsorb heavy metals. It appears that the quartz and mullite were produced from the thermal decomposition of clay minerals, such as kaolinite, during combustion.¹⁹ These results are consistent with previous reports.^{10,19} A broad peak indicating the presence of an amorphous phase due to unburned carbon was observed at about 24°. It can therefore be stated that coal fly ash has an amorphous aluminosilicate nature and its actual composition depends on the variety of coal used, the degree of burning and the method of collection.²⁰

The FTIR spectrum (Figure 2) shows the functional groups that are on the surface of coal fly ash. However, the availability of a particular functional group or binding site does not necessarily guarantee its accessibility as an adsorption site for a metal ion, because of the presence of steric, conformational or other types of barriers. The spectrum displays a number of absorption peaks, of which the band appearing at 1059.0 cm^{-1} is associated with X-O (X = Si, Al) asymmetric stretching vibrations.⁶ Peaks at 1975.7 cm^{-1} and 2363.7 cm^{-1} could be attributed to C=O and alkyl groups, respectively, that are present in the clay material of the coal fly ash. The band appearing at 555.9 cm^{-1} is associated with the octahedral aluminium present in mullite. In addition, bands appearing between 800 cm^{-1} and 600 cm^{-1} are associated with the tetrahedral vibrations formed by what are known as secondary building units and fragments of the aluminosilicate system. These bands are characteristic of the double or single rings (depending on the structure of the material) and/or the XO_4 (X = Si, Al) tetrahedral bonds.²¹ By comparing the spectra before and after adsorption, it becomes clear that the bands before adsorption at 2530.8 cm^{-1} , 2160.5 cm^{-1} , 2028.5 cm^{-1} , 1975.7 cm^{-1} and 1059.0 cm^{-1} shifted after adsorption to 2600.0 cm^{-1} , 2175.7 cm^{-1} , 2036.8 cm^{-1} , 1965.4 cm^{-1} and 1043.5 cm^{-1} , respectively. A shift in all the bands indicates that all functional groups were involved in the adsorption process.

Figure 3 shows the SEM images of coal fly ash before and after adsorption. These images reveal that the raw coal fly ash, that

is the coal fly ash before adsorption, mainly consists of well-developed, smooth, glassy spherical particles (cenospheres) and some irregular-shaped particles interspersed with aggregates of crystalline compounds, which likely correspond to quartz and haematite. Furthermore, the SEM images show low pore development in the coal fly ash. These results are comparable with those reported by El-Naggar et al.⁶ Comparing raw coal fly ash (Figures 3a and 3b) with coal fly ash after adsorption (Figures 3c and 3d), it can be seen that there are morphological changes in the coal fly ash during adsorption. After adsorption, the spheres of coal fly ash were covered by precipitates and complexes formed by the heavy metal ions; similar observations were made by Mohan and Gandhimathi¹⁹.

The textural characteristics and pore structure of coal fly ash are presented in Table 3. The low surface area of coal fly ash is consistent with the SEM images in Figure 3 which show low pore development in coal fly ash. Bayat²² analysed two different

TABLE 3
Textural characteristics and pore structure of coal fly ash

| Textural characteristics | Pore structure |
|---|-----------------------|
| BET surface area, S_{BET} (m^2/g) | 1.73 |
| Micropore specific area, S_{m} (m^2/g) | 1.31 |
| Total pore volume, V_t (cm^3/g) | 2.25×10^{-3} |
| Micropore volume, V_m (cm^3/g) | 1.52×10^{-3} |
| Mesopore volume, V_{me} (cm^3/g) | 7.23×10^{-4} |

BET, Brunauer-Emmett-Teller

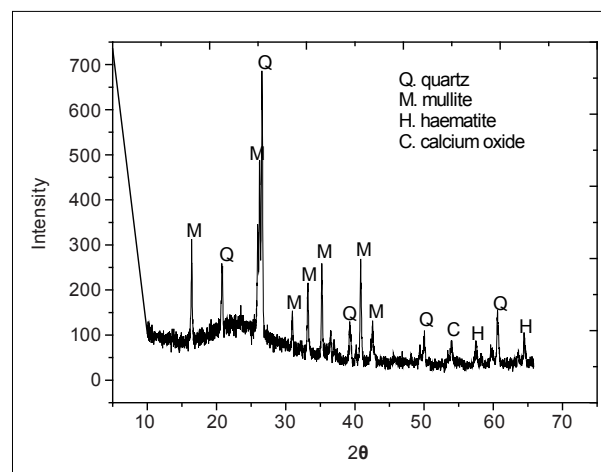


FIGURE 1
The X-ray diffraction profile (diffractogram) of coal fly ash

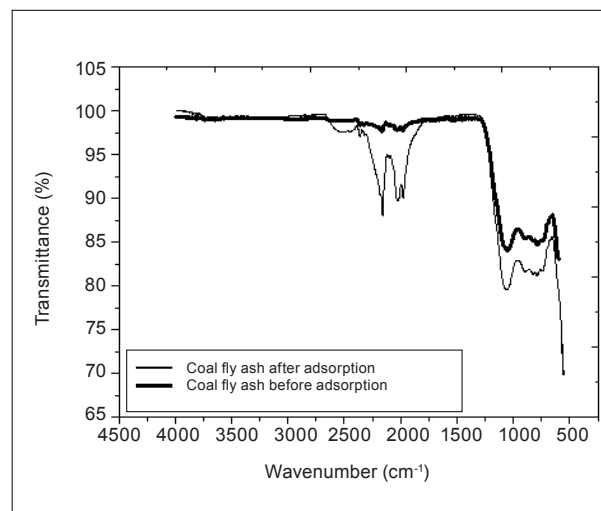
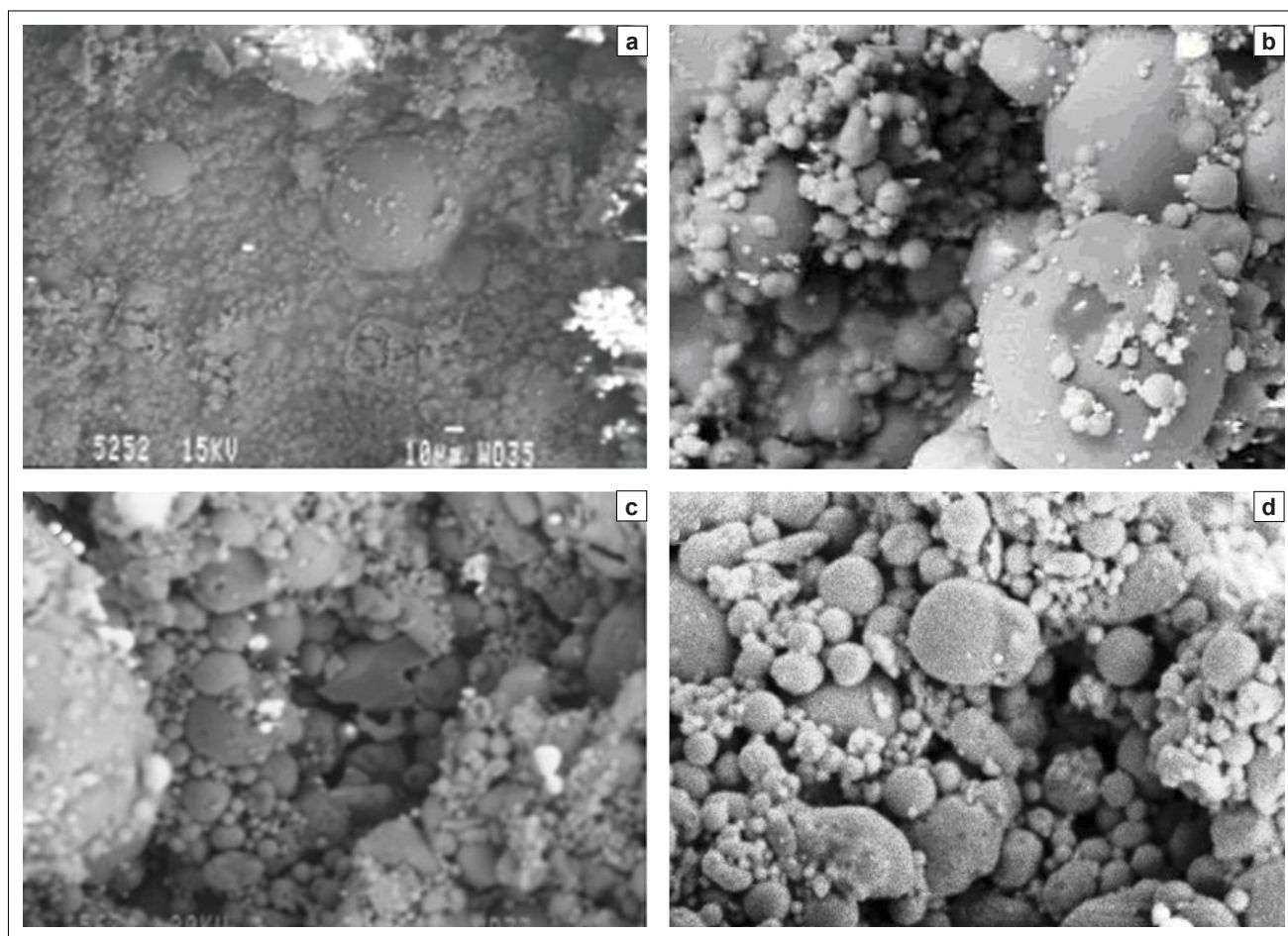


FIGURE 2
Fourier transform infrared spectra of coal fly ash before and after adsorption



400x magnification

FIGURE 3

Scanning electron micrographs of coal fly ash before (a and b) and after (c and d) adsorption

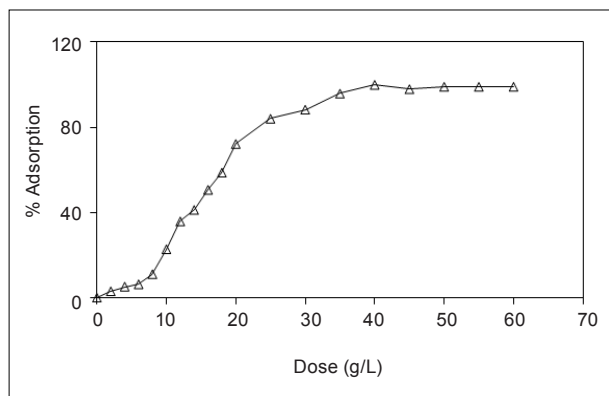


FIGURE 4

Adsorption of cobalt(II) ions as a function of coal fly ash dose at constant pH, temperature, shaking speed and heavy metal and phenol concentrations

Turkish fly ash samples and observed S_{BET} values of less than $0.342 \text{ m}^2/\text{g}$, even lower than those for South African coal fly ash; however, the performance of the two Turkish samples as adsorbents was favourable.

Optimum adsorbent dose

The optimum adsorbent dose was determined by shaking a series of 250-mL flasks containing wastewater with different doses of coal fly ash, varying from 2 g/L to 60 g/L for 4 h. All other factors were kept constant for each flask, according to the zero-level composition shown in Table 1 (i.e. pH = 4, temperature = 25°C , shaking speed = 250 rpm, cobalt = 50 mg/L, other heavy

metals = 50 mg/L and phenol = 110 mg/L). It is observed from Figure 4 that, as the dose of coal fly ash increases, the percentage of cobalt(II) adsorbed increases and reaches a maximum value corresponding to a certain adsorbent dose, above which adsorption will not increase with an increase in adsorbent dose. The minimum adsorbent dose corresponding to the maximum adsorption (100%) is the optimum dose. Thus, it is evident that for the quantitative removal of cobalt(II), the optimum dose of coal fly ash is 40 g/L.

Fitting of a quadratic model for cobalt(II) removal

By applying multiple regression analysis methods, the predicted adsorption capacities of coal fly ash for cobalt(II) ions (q_{co}) can be given as:

$$q_{co} = 1.08 + 0.072x_1 + 0.27x_2 + 0.18x_3 - 0.44x_1^2 - 0.26x_1x_2 + 0.16x_1x_3 + 0.015x_2x_3 \quad [\text{Eqn 4}]$$

where x_1 , x_2 and x_3 are the coded values of the test variables, dose (g/L), pH and initial concentration (mg/L), respectively. The statistical significance of the second order model equation was evaluated using Fisher's *F*-test and an ANOVA and acceptance of the model was made on the basis of a 95% confidence level.²³ Based on probability values less than 0.05, statistical significance was indicated for the model, as well as for the model terms (x_1 , x_2 and x_3) and the interactions between dose and pH (x_1x_2) and between dose and initial concentration (x_1x_3). The interaction between pH and initial concentration (x_2x_3) was not statistically significant.

For a model to be reliable, the response should be predicted with reasonable accuracy when compared with the experimental data.

In this case, there was a high correlation coefficient ($R^2 = 0.9991$) between the predicted values and the real values obtained from the experimental data. Figure 5 shows the three-dimensional response surface plots that are graphical representations of the regression equation, from which the adsorption capacity for different levels of the variables can be predicted. Each response plot represents an infinite number of combinations of two test variables, with the other variable maintained at a constant level.

Combined effects of adsorbent dose and pH

The combined effect of adsorbent dose and solution pH at constant initial concentration was investigated using response surface methodology. Figure 5a reveals that the adsorption of cobalt(II) increased with increasing pH and decreasing adsorbent dose. This trend predicted by the model is consistent with the experimental results shown in Table 2, that is the highest adsorption capacity of 1.118 mg/g was observed at low dose and high pH (run order 7). From our findings, it is apparent that pH has a significant impact on the removal of metals by coal fly ash; these findings are consistent with those reported in the literature.⁹ The pH of solution determines the surface charge of the adsorbent and the degree of ionisation and speciation of the adsorbate. On the surface of the coal fly ash, the functional oxidised groups are present as silica (SiO_2) and haematite (Fe_2O_3). Thus, it will be expected that the cobalt(II) ions will mostly be adsorbed by silica or haematite, or by a combined influence of these oxides; adsorption will also be influenced by the presence of unburned carbon.²⁴ The oxygen atoms on the surface of the silica are free to react with water, which will result in the formation of surface silanol (SiOH) groups. As a result, the surface of the silica is positively charged at low pH and negatively charged at high pH.¹⁹

Other solid materials, such as Fe_2O_3 , exhibit similar patterns in developing positive and negative charges depending on pH.²² At a low pH (i.e. below 2.2, the pH_{pzc} for silica), a positive charge develops on the surface of the coal fly ash resulting in poor adsorption of the metal ions because of repulsion. At pH values above 2.2, the surface of coal fly ash is negatively charged and becomes more negatively charged as the pH increases; the enhanced favourable electrostatic forces results in increased removal of the metal ions. Ricou-Hoeffler et al.²⁵ reported that aluminosilicate compounds in coal fly ash may also be involved in adsorption of metallic ions.

The decrease in adsorption capacity of coal fly ash with an increase in adsorbent dose, could be because of aggregation or overlapping of adsorption sites caused by overcrowding of coal fly ash particles, which results in a decrease in total adsorbent surface available to the metal ions. Particle interaction may also desorb some of the sorbate that is loosely and reversibly bound to the coal fly ash surface.²⁶ Therefore, at high adsorbent doses, some adsorption sites remain unsaturated during the adsorption process because they are not accessible.

Combined effects of adsorbent dose and initial concentration

The relationship between adsorption capacity, dose and initial concentration of cobalt(II) at a constant pH is shown in Figure 5b. It is apparent that the adsorption capacity of coal fly ash increased by increasing the initial concentration and decreasing the adsorbent dose. An increase in cobalt(II) adsorption by increasing the initial concentration is a result of the increase in the driving force of the concentration gradient and not as a direct result of an increase in the initial cobalt(II) ion concentration.^{27,28} Under the same conditions, a higher concentration of cobalt(II) ions present in the solution would cause the active sites of coal fly ash to be surrounded by more cobalt(II) ions; this adsorption process would therefore be carried out more effectively.²⁷ Adsorption capacity is therefore increased by increasing the initial cobalt(II) ion concentration.

Combined effects of pH and initial concentration

The combined effects of solution pH and initial cobalt(II) ion concentration were analysed and it was found that both parameters have an impact on the adsorption capacity of coal fly ash. The model predicted that adsorption of cobalt(II) would increase by increasing the pH and the initial concentration (figure not shown). This prediction is consistent with the experimental results shown in Table 2, wherein the highest adsorption capacities (1.118 mg/g and 1.102 mg/g) were both observed at high pH and high initial concentration (run orders 7 and 8).

Adsorption equilibrium study

Analysis of the adsorption isotherm data is important to develop an equation which accurately represents the results, which could

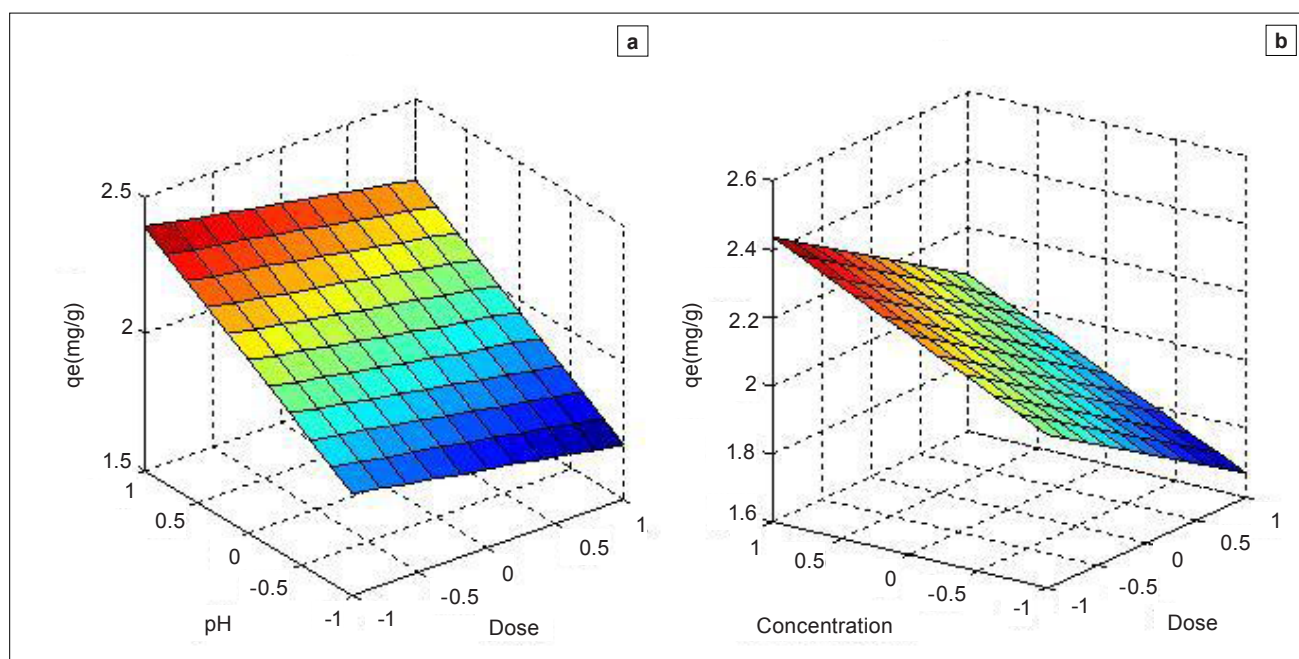
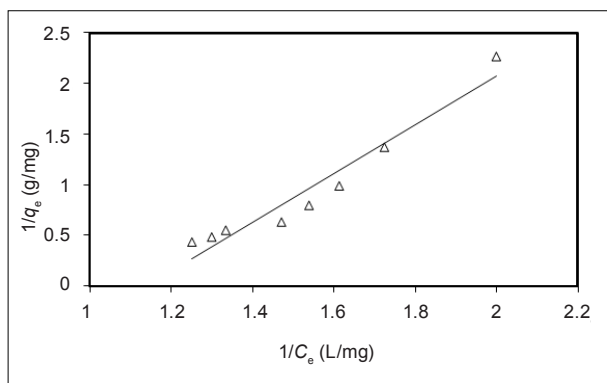


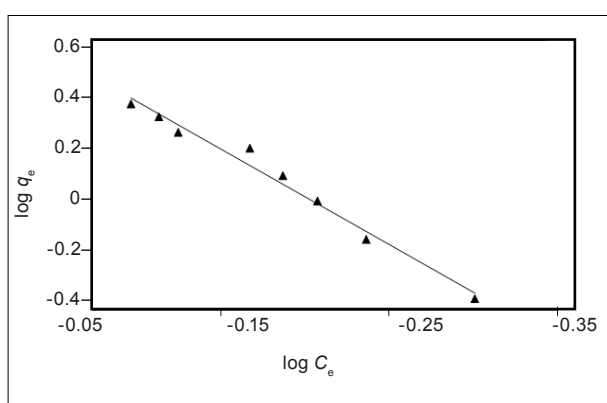
FIGURE 5
Adsorption capacity, q_e , as a function of pH and dose at constant initial concentration (a) and initial concentration and dose at constant pH (b)



q_e , adsorption capacity; C_e , supernatant equilibrium concentration

FIGURE 6

The Langmuir isotherm model for the removal of cobalt(II) ions by coal fly ash



q_e , adsorption capacity; C_e , supernatant equilibrium concentration

FIGURE 7

The Freundlich isotherm model for the removal of cobalt(II) ions by coal fly ash

TABLE 4
Analysis of variance results for the fitted quadratic model for the prediction of cobalt(II) adsorption by coal fly ash

| Source of variation | Sum of squares | Degrees of freedom | Mean square | F-value | p-value |
|---------------------|----------------|--------------------|-------------|----------|----------|
| Model | 2.15 | 7 | 0.31 | 670.46 | < 0.0001 |
| x_1 | 0.04 | 1 | 0.04 | 90.82 | 0.001 |
| x_2 | 0.6 | 1 | 0.6 | 1300 | < 0.0001 |
| x_3 | 0.26 | 1 | 0.26 | 561.75 | < 0.0001 |
| x_1^2 | 0.52 | 1 | 0.52 | 1132.45 | < 0.0001 |
| x_1x_2 | 0.53 | 1 | 0.53 | 1149.78 | < 0.0001 |
| x_1x_3 | 0.21 | 1 | 0.21 | 454.66 | < 0.0001 |
| x_2x_3 | 1.71E-3 | 1 | 1.71E-3 | 3.73 | 0.126 |
| Residual | 1.83E-3 | 4 | 4.58E-4 | - | - |
| Lack of Fit | 1.83E-3 | 1 | 1.83E-3 | 28.23 | - |
| Pure Error | 2.75E-6 | 3 | 9.17E-7 | - | - |
| Total | 2.15 | 11 | - | - | - |

x_1 , adsorbent dose
 x_2 , pH of solution
 x_3 , initial concentration of adsorbate

be used for design purposes and which will optimise an operating procedure. Other researchers in the field of environmental engineering^{29,30} have used Freundlich and Langmuir isotherm equations to represent equilibrium adsorption data despite the fact that these equations have serious limitations on their usage.²⁸ Simplicity and easy interpretability are some of the reasons which would account for the extensive use of these models.

Langmuir isotherm model

The Langmuir isotherm, also called the ideal localised monolayer model, was developed to represent chemisorption. Langmuir³¹ theoretically examined the adsorption of gases on solid surfaces

and considered adsorption as a chemical phenomenon. The Langmuir equation relates the coverage of molecules on a solid surface to concentration of a medium above the solid surface at a fixed temperature. This isotherm is based on the assumptions that^{18,32}:

- adsorption is limited to monolayer coverage
- all surface sites are alike and can only accommodate one adsorbed molecule
- the ability of a molecule to be adsorbed on a given site is independent of its neighbouring sites' occupancy
- adsorption is reversible
- the adsorbed molecule cannot migrate across the surface or interact with neighbouring molecules.

By applying these assumptions and the kinetic principle (i.e. the rates of adsorption and desorption from the surface are equal), the Langmuir equation can be written in the following hyperbolic form:

$$q_e = q_{\max} \frac{K_L C_e}{1 + K_L C_e} \quad [\text{Eqn 5}]$$

This equation is often written in different linear forms³²:

$$\frac{1}{q_e} = \left[\frac{1}{K_L q_{\max}} \right] \frac{1}{C_e} + \frac{1}{q_{\max}} \quad [\text{Eqn 6}]$$

$$\frac{C_e}{q_e} = \frac{1}{q_{\max}} C_e + \frac{1}{K_L q_{\max}} \quad [\text{Eqn 7}]$$

where q_e is the adsorption capacity at equilibrium (mg/g), q_{\max} is the theoretical maximum adsorption capacity of the adsorbent (mg/g), K_L is the Langmuir affinity constant (L/mg) and C_e is the supernatant equilibrium concentration of the system (mg/L). The Langmuir constants are predicted from the plot of $1/q_e$ versus $1/C_e$ which is shown in Figure 6 for cobalt(II) removal using coal fly ash. From this plot, the maximum adsorption capacity is 0.401 mg/g, the Langmuir affinity constant is 1.000 L/mg and the correlation coefficient is 0.9390.

Freundlich isotherm model

The Freundlich isotherm is originally of an empirical nature, but has since been used as a model for interpretation of adsorption to heterogeneous surfaces or surfaces supporting sites of varied affinities. It is assumed that the stronger binding sites are occupied first and that the binding strength decreases with increasing degree of site occupation. According to this model, the adsorption capacity can be expressed by a power law function of the solute concentration as follows:

$$q_e = K_F C_e^{1/n} \quad [\text{Eqn 8}]$$

where K_F is the Freundlich constant related to adsorption capacity (mg/g) and n is the heterogeneity coefficient (dimensionless). For linearisation of the data, the Freundlich equation is written in logarithmic form:

$$\log q_e = \log K_F + (1/n) \log C_e \quad [\text{Eqn 9}]$$

The plot of $\log q_e$ versus $\log C_e$ has a slope with the value of $1/n$ and an intercept magnitude of $\log K_F$. On average, a favourable adsorption tends to have a Freundlich constant, n , between 1 and 10. A larger value of n (i.e. a smaller value of $1/n$) implies a stronger interaction between the adsorbent and the adsorbate.³³ Figure 7 provides results on Freundlich isotherm fittings for the removal of cobalt(II) by coal fly ash. The Freundlich constants, i.e. K_F and n , were found to be 5.611 mg/g and 0.276 mg/g, respectively. The correlation coefficient was higher ($R^2 = 0.9810$) than that obtained for the Langmuir isotherm ($R^2 = 0.9390$), indicating the applicability of the Freundlich isotherm to the adsorption data. This observation is consistent with the heterogeneous nature of coal fly ash, that is the presence of different groups of surface adsorption sites such as $\equiv\text{SiOH}$ and $\equiv\text{FeOH}$. Similar observations were reported by Cho et al.⁹ for the adsorption of zinc, lead, cadmium and copper using coal fly ash.

After using it as an adsorbent, coal fly ash can be employed as a filling material in pavement linings, soil stabilisation, cement and concrete industries and can be disposed of in a landfill.¹⁸

CONCLUSION

South African coal fly ash was used successfully to remove cobalt(II) ions from synthetic petrochemical wastewater. The interactive effects of adsorbent dose, solution pH and initial concentration were investigated using RSM and a second order response surface model equation to describe the adsorption of cobalt(II) ions was derived. In terms of the models used in this study, the adsorption process was better described by the Freundlich isotherm model than the Langmuir model. Nonetheless, assessment of the interactive effects of process variables revealed that the system was sensitive to the tested process variables and was deemed technically feasible.

Leaching of coal fly ash may potentially result in extraction of some environmental pollutants. The multi-element analysis of the treated wastewater therefore needs to be investigated further in order to determine any available leachates. Moreover, the actual concentration of the leachates must be determined to ascertain if it is below or above the maximum allowable limits.

The results presented from this study can help to design an appropriate environmental management strategy to minimise the adverse impacts caused by industrial wastewater contaminated with cobalt(II) ions. We conclude that South African coal fly ash, being a natural, abundant and low-cost adsorbent, might be a suitable local alternative for elimination of cobalt(II) from aqueous solutions.

ACKNOWLEDGEMENTS

The authors wish to acknowledge Lethabo Power Station (South Africa) for supplying the coal fly ash used in this study.

REFERENCES

- Rengaraj S, Moon SH. Kinetics of adsorption of Co(II) removal from water and wastewater by ion exchange resins. *Water Res.* 2002;36:1783–1793.
- Cavaco SA, Fernandes S, Quina MM, Ferreira LM. Removal of chromium from electroplating industry effluents by ion exchange resins. *J Hazard Mater.* 2007;144:634–638.
- Kim H, Baek K, Lee J, Iqbal J, Yang J. Comparison of separation methods of heavy metal from surfactant micellar solutions for the recovery of surfactant: Desalination. 2006;191:186–192.
- Mavrov V, Stamenov S, Todorova E, Chmiel H, Erwe T. Removal of nickel ions from wastewater by Mg(OH)₂/MgO nanostructures embedded in Al₂O₃ membranes. *J Alloys Compd.* 2006;426:281–285.
- Kurt K, Apaydin O, Gonullu MT. Reduction of COD in wastewater from an organized tannery industrial region by Electro-Fenton process. *J Hazard Mater.* 2007;143:33–40.
- El-Naggar MR, El-Kamash AM, El-Dessouky MI, Ghonaim AK. Two-step method for preparation of NaA-X zeolite blend from fly ash for removal of cesium ions. *J Hazard Mater.* 2008;154:963–972.
- Reynolds K, Kruger R, Rethman N, Truter W. The production of an artificial soil from sewage sludge and fly-ash and the subsequent evaluation of growth enhancement, heavy metal translocation and leaching potential. *Water SA.* 2002;Special Edition: WISA Proceedings:73–77.
- Woolard CD, Petrus K, Van der Horst M. The use of modified fly ash as an adsorbent for lead. *Water SA.* 2000;26:531–536.
- Cho H, Oh D, Kim K. A study on removal characteristics of heavy metals from aqueous solution by fly ash. *J Hazard Mater.* 2005;B127:187–195.
- Potgieter JH, Bada SO, Potgieter-Vermaak SS. Adsorptive removal of various phenols from water by South African coal fly ash. *Water SA.* 2009;35:89–96.
- Bas D, Bayaci IH. Modeling and optimization I: Usability of response surface methodology. *J Food Engin.* 2007;78:836–845.

- Elibol M. Response surface methodological approach for inclusion of perfluorocarbon in actinorhodin fermentation medium. *Process Biochem.* 2002;38:667–773.
- Annadurai G, Juang RS, Lee DJ. Adsorption of heavy metals from water using banana and orange peels. *Water Sci Technol.* 2003;47:185–190.
- Zhu Z, Li A, Yan L, Liu F, Zhang Q. Preparation and characterization of highly mesoporous spherical activated carbons from divinylbenzene-derived polymer by ZnCl₂ activation. *J Colloid Interface Sci.* 2007;316:628–634.
- Patel H, and Madamwar D. Effects of temperatures and organic loading rates on bio-methanation of acidic petrochemical wastewater using an anaerobic upflow fixed-film reactor. *Bioresour Technol.* 2002;82:65–71.
- Pollution Prevention and Abatement Handbook. World Bank Group Environmental, Health and Safety General Guidelines [homepage on the Internet]. c1998 [cited 2009 Feb 02]. Available from: <http://www.scribd.com/doc/12239840/Pollution-Prevention-Abatement-Handbook-1998>
- Al-Degeys YS, El-Barghouthi MI, Issa AA, Khraisheh MA, Walker GM. Sorption of Zn(II), Pb(II) and Co(II) using natural sorbents: Equilibrium and kinetic studies. *Water Res.* 2006;40:2645–2658.
- Sarkar M, Acharya PK. Use of fly ash for the removal of phenol and its analogues from contaminated water. *Waste Manag.* 2006;26:559–570.
- Mohan S, Gandhimathi R. Removal of heavy metal ions from municipal solid waste leachate using coal fly ash as an adsorbent. *J Hazard Mater.* 2009;169:351–359.
- Sen AK, De AK. Adsorption of mercury(II) by coal fly ash. *Water Res.* 1987;21:885–888.
- Jime'nez AF, Palomo A. Mid-infrared spectroscopic studies of alkali-activated fly ash structure. *Microporous Mesoporous Mater.* 2005;86:207–214.
- Bayat B. Comparative study of adsorption properties of Turkish fly ashes: II. The case of chromium (VI) and cadmium (II). *J Hazard Mater.* 2002;95:275–290.
- Bhatia S, Wong CT, Abdullah AZ. Optimization of air-borne butyl acetate adsorption on dual-function Ag-Y adsorbent-catalyst using response surface methodology. *J Hazard Mater.* 2009;164:1110–1117.
- Panday KK, Prasad G, Singh VN. Copper (II) removal from aqueous solutions by fly-ash. *Water Res.* 1985;19:869–873.
- Ricou-Hoeffler P, Lecuyer I, Le Cloirec P. Experimental design methodology applied to adsorption of metallic ions onto fly ash. *Water Res.* 2001;35:965–976.
- Shukla A, Zhang Y, Dubey P, Margrave JL, Shukla SS. The role of sawdust in the removal of unwanted materials from water. *J Hazard Mater.* 2002;B95:137–152.
- Han H, Li Y, Li J, Zhang HX, Shi J. Biosorption of copper and lead ions by waste beer yeast. *J Hazard Mater.* 2006;137:1569–1576.
- Srivastava VC, Swamy MM, Mall ID, Prasad B, Mishra IM. Adsorptive removal of phenol by bagasse fly ash and activated carbon: Equilibrium, kinetics and thermodynamics. *Colloids Surf A Physicochem Eng Asp.* 2006;272:89–104.
- Ho Y. Selection of optimum sorption isotherms. *Carbon.* 2004;42:2113–2130.
- Basha S, Murphy ZVP, Jha B. Sorption of Hg(II) from aqueous solutions onto *Carica papaya*: Application of isotherms. *Ind Eng Chem Res.* 2008;47:980–986.
- Langmuir I. The adsorption of gases on plane surfaces of glass, mica and platinum. *J Am Chem Soc.* 1918;40:1361–1403.
- Febrianto J, Kosasih AN, Sunarso J, et al. Equilibrium and kinetic studies in adsorption of heavy metals using biosorbent: A summary of recent studies. *J Hazard Mater.* 2009;162:616–645.
- Site AD. Factors affecting sorption of organic compounds in natural sorbent/water systems and sorption coefficients for selected pollutants: A review. *J Phys Chem Ref Data* 2001;30:187–439.