

Evaluation of a wind farm project for a smart city in the South-East Coastal Zone of Mauritius

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Abstract

A study was carried out to analyse the potential of wind energy in the generation of electricity for a smart city which is located in the South-East Coastal Zone of Mauritius. A flat land area of 10 square km situated about 3.5 km from the smart city was chosen for the placement of a wind farm. The viability of the location was assessed by analysing ten years (Jan 2005 to Dec 2014) of mean hourly wind speed measured at a height of 10 m above ground level (m.a.g.l). The speed data was filtered according to the AWS (1997) guidelines and computed at 60 m.a.g.l using the power law formula. At this height, the average wind speeds was approximately 6.5 m/s, which was considered cost effective, as per the European Wind Energy Union guidelines for the harvesting of wind power. Estimated yearly power generated by a wind farm consisting of 40 wind turbines, each of rating capacity 275 kW, placed at a hub height of 60 m were made. The study resulted in an investment proposal for a 11 MW wind farm project in Mauritius.

Keywords: wind energy assessment, two-parameter weibull distribution, wind power, wind turbines

1. Introduction

Energy is the basis of the world's economy, combining with all other entities that are vital for economies. The quest to meet growing energy demand of the global population initiated numerous research in a wide range of environmental application of renewable energy (RE) (Park & Law, 2015). Currently, the wind sector stands out as one of the most promising RE as wind is an inexhaustible diurnal resource that can provide significant quantities of energy to support the needs of a country (Ackerman & Soder, 2002). Exploitation of wind energy for the production of electricity increased around the world at an accelerating pace more than ten 10 years ago (Marcukaitis *et al.*, 2008). Wind energy is currently being exploited widely in many countries such as the USA, Germany, Spain, China, India, UK, Denmark and Canada (Adelaja *et al.*, 2012; Coskun & Turker, 2012). According to the American Wind Energy Association (AWEA) and the European Wind Energy Association (EWEA), cumulative global wind energy generating capacity exceeded 282 GW in 2012, with an increase of about 80% of new capacity that was installed worldwide during the past decade (WEC, 2014). Such a vast RE resource has a potential to be exploitable by small island developing states (SIDS) such as the island of Mauritius. The work of Dhunny *et al.* (2015) showed the potentials of wind energy for Mauritius at different locations comparable with those of countries already reaping the benefits of this technology.

An accurate wind resource assessment is an important and critical factor to be well understood for harnessing the power of the wind (Marcukaitis *et al.*, 2008). The identification of potential areas

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that might be suitable for the development of wind projects are enhanced by accurate wind resource data available at specific chosen locations (Radics & Bartholy, 2008). In its budget speech for the financial year 2015-2016, the Government of Mauritius clearly indicated its vision to build up eight smart cities throughout the island. These are Omnicane Mon-Tresor Airport City in the South East Coastal Zone, St-Felix Village Project in the South, Medine Integrated Park in the West, Azuri phase 2 and Terra Projects in the North, Riche-Terre and Highlands Project in the centre and Roches-Noires in the North-East Coastal Zone. The smart cities are expected to produce a significant amount of the energy of their own using RE sources such as solar and wind. In this work, the potential of wind energy was assessed for one of the smart cities, the Omnicane Mon Tresor Airport. The placement of a potential wind farm is also analysed along with the expected power output yielded at that location to furnish the smart city as well as the project costing in terms of initial investment and expected return on investment.

Section 2 discusses the wind assessment method utilised. Section 3 describes the general wind flow patterns over Mauritius, as well as the site of interest where data was collected for this study. In Section 4, the main results obtained are analysed and discussed. Section 5 enumerates the project cost and Section 6 outlines the main conclusions of this work.

2. Wind energy assessment

The assessment of wind energy potential of a region requires long term data related to the wind speed and an accurate determination of its distribution. The variations in wind speed can be characterised by two functions, namely, the probability density function (PDF) and the corresponding cumulative density function (CDF). In literature, the wind speed frequency distribution for a given location was represented by different and various PDFs such as Burr, Weibull, Lognormal, Normal, Rayleigh, Gamma and Frechet (Kollu *et al.*, 2012; Morgan *et al.*, 2010; Abbas *et al.*, 2012; Masseran *et al.*, 2013). Dhunny *et al.* (2014) performed a statistical analysis on the wind speed data of the two meteorological stations, Plaisance and Vacoas. The authors undertook to fit their data with these PDFs and compared the results using the Chi-Square, Kolmogorov and Anderson-Darling goodness-of-fit tests. The results indicated that both sets of wind speed data were more significantly represented by the Weibull and Burr distributions. For this study, the Weibull distribution was solely considered. A review of the wind assessment literature revealed that the Weibull PDF fits most accurately a variety of wind speed data measured at different geographical locations in the world (Carta *et al.*, 2009;

Altunkaynak *et al.*, 2012). Moreover, by finding the shape parameter and scale factor of the Weibull distribution that represents the wind speed data, direct estimates of the expected wind power can be made (Mirghaed & Roshandel, 2013). During the last decade, research was undertaken on the wind characteristics and wind power potential in many countries around the world (Tarkowski & Uliasz-Misiak, 2003). Examples include Tunisia (Zghal *et al.*, 2011), eastern Mediterranean (Sahin *et al.*, 2005), Turkey (Gokcek *et al.*, 2007a; Ucar & Balo, 2009b) Nigeria (Ngala *et al.*, 2006), Iran (Keyhani *et al.*, 2010), Columbia (Jimenez *et al.*, 2011), Egypt (Shata & Hanitsch, 2006), Kuwait (Al-Nassar *et al.*, 2007), coastal areas of Jiwani, Pakistan (Lehri *et al.*, 2013) and Greece (Kaldellis, 2002) among others.

2.1 The Weibull PDF

Knowledge of the wind speed frequency distribution plays an important role for the estimation of wind potential in any location (Azad *et al.*, 2014). When the distribution of wind speed is known, both the wind power potential and economic viability of the site can be calculated. The two-parameter Weibull distribution $f(v)$, most commonly known for its high accuracy for wind speed data analysis (Zghal *et al.*, 2011), is expressed as Equation 1.

$$f(v) = \frac{k}{c} \left(\frac{v}{c} \right)^{k-1} \exp \left[-\left(\frac{v}{c} \right)^k \right], \quad (1)$$

where c is the Weibull scale parameter (same dimension as v), which indicates the wind regime at that location and k is a dimensionless Weibull shape parameter (Abed & El-Mallah, 1997). The cumulative distribution function $F(v)$, which is the integral of $f(v)$ in the range of $(0, v)$, is expressed according to Equation 2.

$$F(v) = 1 - \exp \left[-\left(\frac{v}{c} \right)^k \right]. \quad (2)$$

The mean and variance are respectively given by Equations 3 and 4:

$$\bar{v} = E(v) = c \Gamma(1 + 1/k), \quad (3)$$

$$\text{Var}(v) = c^2 \left[\Gamma(1 + \frac{2}{k}) - \Gamma^2(1 + \frac{1}{k}) \right], \quad (4)$$

where Γ is the gamma function. To estimate the parameters k and c for a given set of measured velocity data, numerous methods were proposed in the literature (Mann *et al.*, 1974). The most common one is the Maximum Likelihood Estimation (MLE), of which details about the method is found in the work of Harris & Stocker (1998).

2.2 Wind speed variation with altitude

As wind turbine can be placed at different heights, the wind speed data need to be measured at such heights by using the power law which is one of the most accepted expression in the literature (Zekai Sen & Erdik, 2012). This law describes the vertical variation of wind speed and represented by Equation 5.

$$v(h) = v_0 \left(\frac{h}{h_0} \right)^\alpha, \quad (5)$$

where $v(h)$ is the wind speed at the hub height h , v_0 is the wind speed at measured height and α , wind shear power law exponent. The value for α varies from 0.1 over the tops of steep hills to 0.25 in sheltered locations. For flat coastal regions, α is taken as 0.143 (1/7), which is the typical value used in most research (Youm *et al.*, 2005).

As the wind velocity varies with height, it is evident that the Weibull parameters also change with height. Oyedepo *et al.* (2012) provide the expressions given by Equations 6 and 7:

$$c(h) = c_0 \left(\frac{h}{h_0} \right)^\alpha, \quad (6)$$

and

$$c(h) = c_0 \left(\frac{h}{h_0} \right)^\alpha, \quad (7)$$

where c_0 and k_0 are respectively the scale factor and shape parameter at the measured height h_0 .

2.3 Estimation of wind power density and annual energy output from a wind turbine

The wind power $P_{wind}(v)$ that can be captured by a wind turbine is given by the product of the mass flow rate entering the rotor blades of the wind turbine and the kinetic energy per unit mass in the wind. It is estimated by Equation 8.

$$c(h) = c_0 \left(\frac{h}{h_0} \right)^\alpha, \quad (8)$$

where ρ is the mean air density (assumed to be 1.225 kg/m in this study), the A is the swept area of the rotor blades and the v is the wind speed. As stated by Ettoumi *et al.* (2008), the instantaneous electrical energy $W(v)$ generated by a wind turbine depends on the efficiency and the instantaneous local wind speed and is given as Equation 9.

$$c(h) = c_0 \left(\frac{h}{h_0} \right)^\alpha, \quad (9)$$

where $g(v)$ (as given by the manufacturer) is the efficiency of the turbine at speed v . The mean annual

energy output of the wind turbine is given by Equation 10.

$$v(h) = v_0 \left(\frac{h}{h_0} \right)^\alpha, \quad (10)$$

where N_h is the number of hours in a year and v_{in} and v_{out} are the cut-in and cut-off wind speeds of the turbine respectively (Jimenez *et al.*, 2011).

2.4 Turbulence

The dissipation of the wind's kinetic energy into thermal energy causes turbulence in the wind. Turbulent wind have a moderately steady mean over time periods of approximately an hour. But over short times it has quite a big disparity. Turbulence can be considered as the arbitrary wind speed fluctuations imposed on the mean wind speed, which occurs in all three 3 directions: longitudinal, tangential and vertical. It is important to note that existence of turbulence decreases the power and causes a fatigue stress in the wind turbine (Oh *et al.*, 2012; Mirhosseini *et al.*, 2011).

2.4.1 Turbulence intensity

Turbulence intensity is the ratio of the standard deviation of the wind speed to the mean (Manwell *et al.*, 2002). As stated before, the length is in the vicinity of one hour. Turbulence intensity changes with the mean wind speed, the surface roughness, the atmospheric stability and the topographic features (Frost *et al.*, 1978). The International Electrotechnical Commission (IEC) (IEC, 2005; IEC, 2008) defines turbulence intensity into different classes for wind turbine constructions.

3. Site description and data collection

The island of Mauritius is found at the edge of the tropics, situated below the equator, at the latitude 2017' south and longitude 5750' east (see Figure 1). This island is of volcanic origin and forms part of the Mascarene islands. The main land of Mauritius spans over 60 km in the north-south direction and 45 km in the east-west direction. Due to its geographical location, Mauritius is influenced by two types of wind: the South East Trade Winds and the Westerlies. The south hemisphere trades are stronger than the northern ones. This is due to the larger areas of land along with their frictional effects in the northern part of the island. In the hottest months of the Northern Hemisphere, a low-level cross-equatorial flow is experienced in the western Indian Ocean. This wind can reach 1000–1500 m above the surface, though in April the flow is weak and nearly disappears in May (Padya, 1989). The Westerlies originate during the Monsoon times in India during June, and their presence are felt in Mauritius, during that period that corresponds to winter season (Padya, 1989). Mostly year round,

the island is influenced by the South East Trade Winds with higher speeds because the land mass in the south occupies less area compared with the North. The trade winds blow mostly from the south-east in the southern hemisphere, strengthening during the winter and when the Arctic oscillation is in its warm phase. At 1000 m, the trade winds attain their highest average value during the months of August and September, while their strength in the whole of winter is high as compared to summer. The presence of some Easterlies during the months of June to October could also be experienced. The prevailing trade winds over the island blow predominantly from the east with an average speed of 5 m/s at 10 m above ground level. Occasionally, during the peak winter months of July and August, with the passage of strong anticyclones, wind gusts are likely to reach more than 25 m/s in some exposed areas (Padya, 1989).

Figure 1 also shows the locations of the proposed smart cities. The Mon Tresor Airport Smart City (proposed schema shown in Figure 2), is to be located in the south-eastern part of the island in the region of Plaisance that comprises the SSR International Airport and mainly sugarcane plantations and some settlement areas.

This study utilises hourly wind data measured at Plaisance at 10 m above ground level. Data obtained were from January 2005 to December 2014. The AWS (1997) wind resource assessment handbook was used as a guide for data filtering. The data, at 10 m hub height were checked thoroughly for homogeneity, outliers and missing records before being processed for the study. Errors and missing data as well as wind gusts and cyclonic winds (wind exceeding 20 m/s) were eliminated.

Hence this study was restricted to flow of wind for normal days. The monthly averages of the filtered data, computed for height of 60 m above ground level (60 m.a.g.l) using Equation (5), are displayed in Figure 3. It can be observed that the average wind speeds vary between 4.9 m/s and 6.2 m/s with the maximum wind speed in August and September (Winter season) while the minimum wind speed occurred in December, February and May, which correspond to the summer season. The maximum turbulence intensity is 1.8 for 60 m and the average is 0.12 (turbulence intensity is a dimensionless quantity).

3.1 Wind Farming near an airport

The Mon Tresor Airport smart city is planned to be built in the vicinity of the SSR international Airport. As shown in Figure 4, a relatively flat location is proposed for the setting up of a wind farm to furnish the smart city, which is a region with an area of 10 km². A recent study by Dhunny *et al.* (2015), based on CFD analysis of wind flow patterns showed that this region has a great potential for wind farming. The airport is approximately 3.6 km away from the proposed wind farm location. Consequently, it is important to consider the effect of the wind farm on radar as well as safety risks caused by the wind turbines acting as large physical obstructions to aeroplanes.

According to the Civil Department of Aviation of Mauritius (Airspace & Group, 2013), in the south-east region the lower flight altitude limit of planes and helicopters is 1100 m. The Federal Aviation Administration (FAA) in the United States and its European equivalent suggest that near an airport, hub heights of wind turbines should not exceed

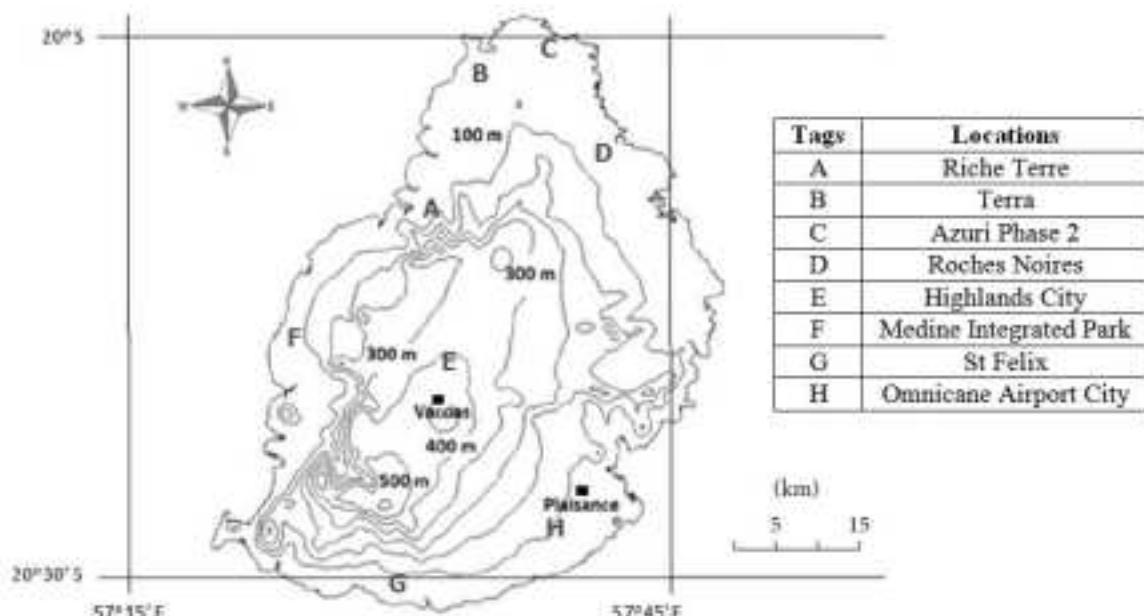


Figure 1: A map of the main island of Mauritius showing the locations of the smart cities and their respective elevations above sea level



Figure 2: Mon Tresor Airport Smart City (proposed schema)
(Smart City, 2015)

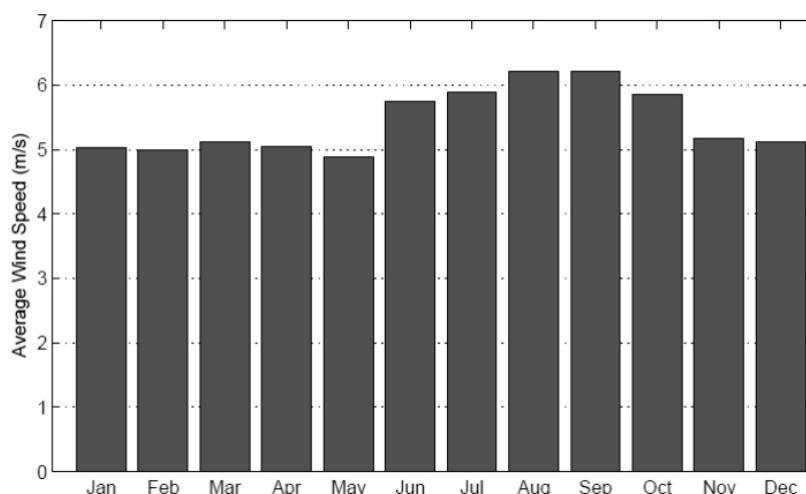


Figure 3: Monthly average wind speed (m/s) at Plaisance (60 m.a.g.l) from 01 January 2005 to 31 December 2014

60 m above ground level. Figure 4 also shows the different surfaces measured from the runway, in which there are restrictions on heights of buildings according to the FAA. It is evident that the proposed wind farm is partially located within the boundaries of the Outer Horizontal Surface in which the buildings heights should not be more than 100 m.a.g.l. Therefore, as per the existing regulations, if the wind farm consisted of turbines with hub height up to 60 m and rotor radius not exceeding 30 m, it should have no effect on the airspace reserved for aircraft operations.

To avert interference with the airport radar, the FAA proposes that a safety distance of 10 km should be retained. Since the current location of the radar is about 3 km from the boundary of the wind farm, it can be re-located at the outer extreme edge of the airport area, which will satisfy the FAA regulations for radar placement from a wind farm.

3.2 Wind turbine arrays

The design of wind farms as well as the exact locations of the wind turbines have to be meticulously planned to prevent power losses due to wake effects (Park & Law, 2015). Numerous technical issues arise with the close spacing of multiple wind turbines (Lissaman *et al.*, 1982). The most important ones are related to the question of the optimum location of the wind turbines and the spacings. The installation needs to be done in such a way as to maximize the energy obtained from the wind equipments and to cram as much wind turbines as possible. According to Manwell *et al.* (2002), the closer the wind turbines are towards each other, the more the energy captured will be reduced. This is due to the fact that the extraction of energy by those wind turbines that are upwind of other turbines results in a decrease in wind speeds at the downwind turbines and increased turbulence. Consequently, these

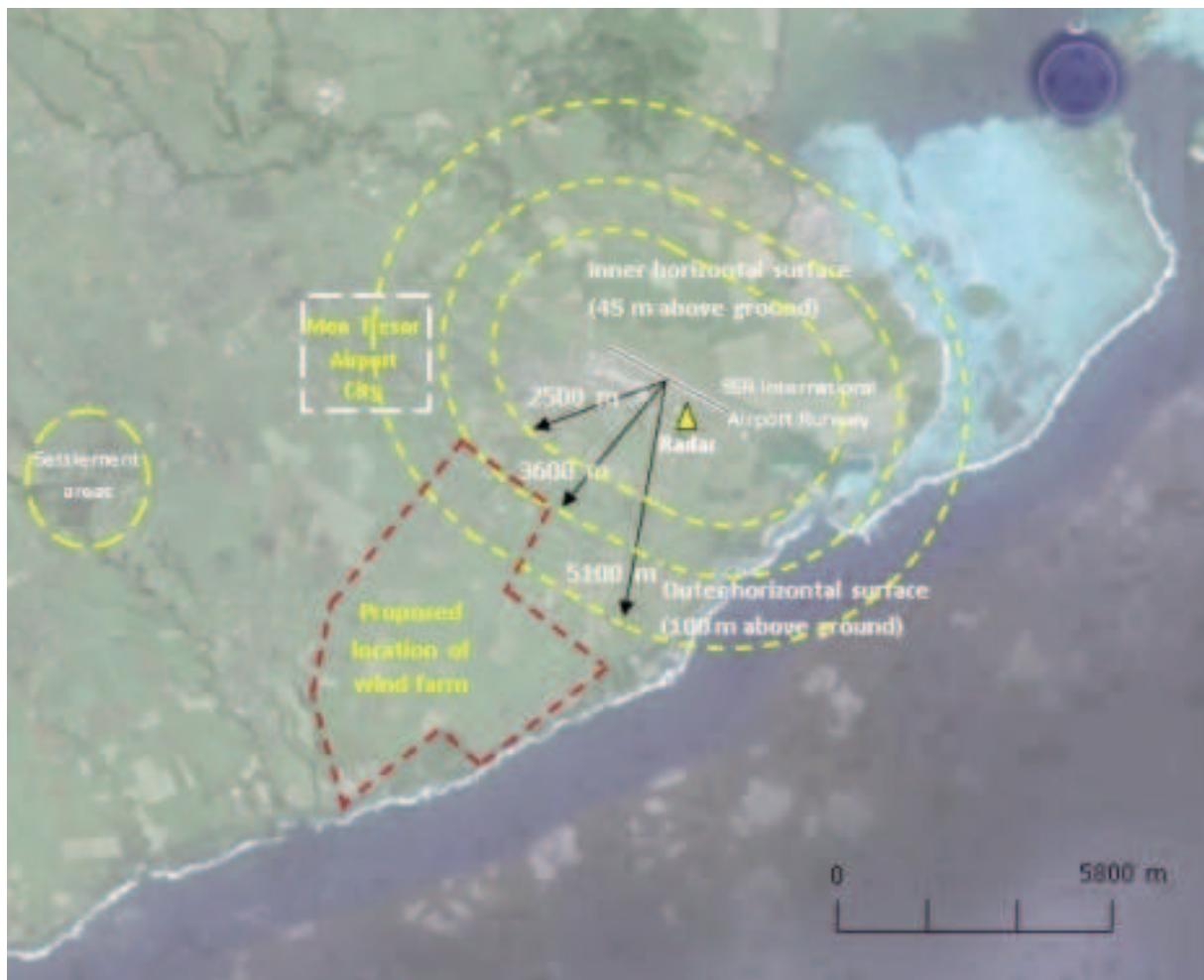


Figure 4: Part of the aeronautical chart for SSR airport, including edges of the applicable obstacle limitation surfaces and the location of the proposed wind farm

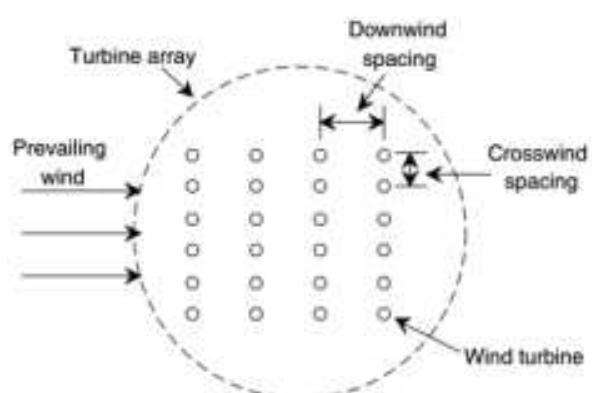


Figure 5: Wind farm array schematics
(adapted from Manwell *et al.* (2002))

wake effects decrease the energy production. Figure 5 illustrates the ideal placement of wind turbine arrays with respect to the prevailing wind direction according to Manwell *et al.* (2002). Lissaman *et al.* (1982) have shown that for turbines spaced 8 to 10D apart in the downwind direction and 5 apart in the cross wind direction (where D is the turbine diameter), the array losses are less than 10%. Therefore,

in the proposed wind farm area (zoomed in Figure 6), on respecting the above mentioned constraints, a total of forty wind turbines can be easily accommodated.

3.3 Choice of the wind turbine

Wind turbines of hub height 60 m and rotor radius of up to 30 m has capacity in the range of 225 to 300 kW (IRNA, 2012). The most popular turbines falling in this category are: NTK 250 kW, Vestas 225 kW, KWT 300 kW, Nord Tank 300 kW and the Vergnet GEV MP 275 kW. Their main characteristics are given in Table 1.

Table 1: Main features of selected wind turbines

Wind turbine model	Rotor diameter (m)	Power rating (kw)	Country
NTK	28	250	UK
Vestas	27	225	Denmark
KWT	33	300	Japan
Nord Tank	54	300	Denmark
Vergnet	30	275	France

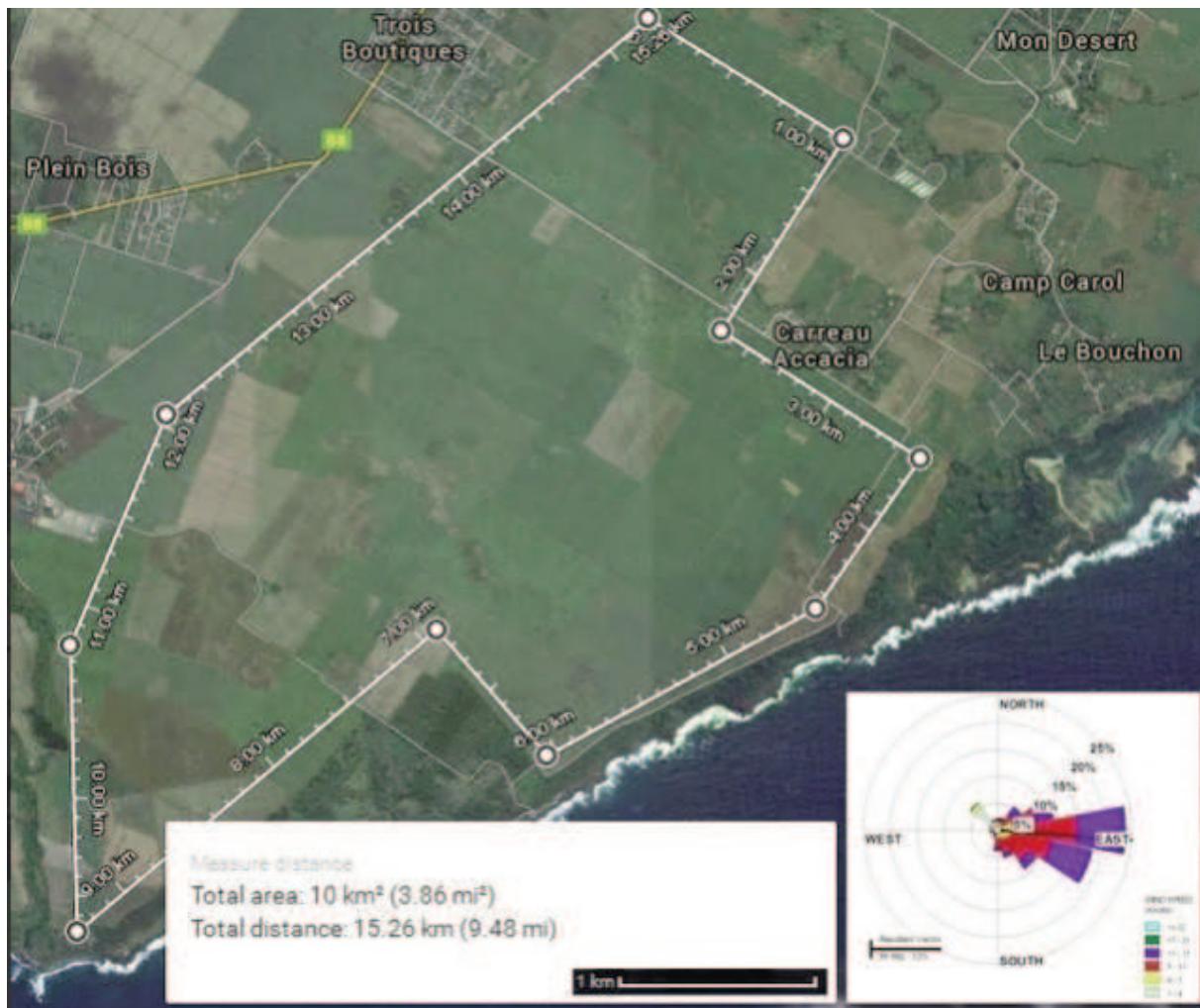


Figure 6: Zoom of the proposed wind farm location showing its perimeter and area, nearby 'small' settlement areas and the prevailing wind direction

The Vergnet GEV MP 275 kW wind turbine was selected as it is specially designed for operation in tropical countries. This particular wind turbine has already been utilised for wind farming in the tropical islands of Rodrigues and Reunion. In Rodrigues, a wind farm consisting of four such turbines was set up at Trefles and two turbines at another location, Grenade. For Reunion, fifteen such turbines were erected for wind farming in 2004 and another eight were added in 2006. Detailed characteristics of the Vergnet GEV MP 275 kW wind turbine and the power curve as given by the manufacturer in the turbine's manual, are given in Table 2 and Figure 7.

Table 2: Characteristics of the Vergnet 275 kW wind turbine

Rated power (kw)	275
Swept area (m ²)	804
Rotor diameter (m)	32
Cut-in wind speed (m/s)	3.5
Cut-off wind speed (m/s)	25
Rated wind speed (m/s)	12

4. Analysis and discussion

The methodology discussed in Section 3 was applied to the wind data. Results obtained are analysed and discussed in the following sections.

4.1 Annual and seasonal probability density of wind speeds

The probability distribution of wind speed is needed in evaluating the potential of wind power at the wind farm location. Figure 7 shows the 10-year annual and seasonal (summer and winter) mean histograms of recorded wind speeds along with fitted Weibull wind speed distributions at 60 m.a.g.l. The corresponding average value of the data and the Weibull *c* and *k* values are also displayed. The observed frequency for the annual curve rises steadily reaching a maximum value for wind speed of 5 m/s, and then drops gradually. For the summer season, the observed frequency reaches a maximum at 5.5 m/s and for the winter case peaks at 6.5 m/s. In all cases, the Weibull curves peak near the average values of the wind speeds. The similarity of the trends shows a good representation given by the Weibull model when compared to the actual data.

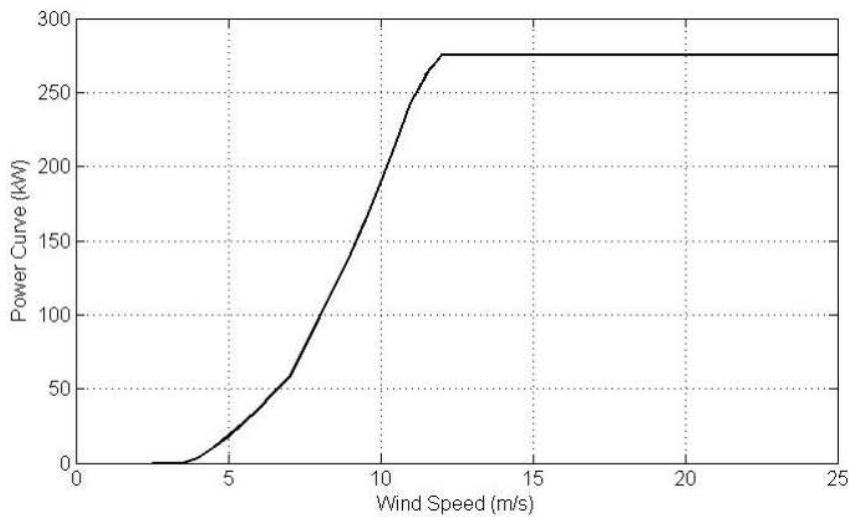


Figure 7: The power curve according to the manufacturer

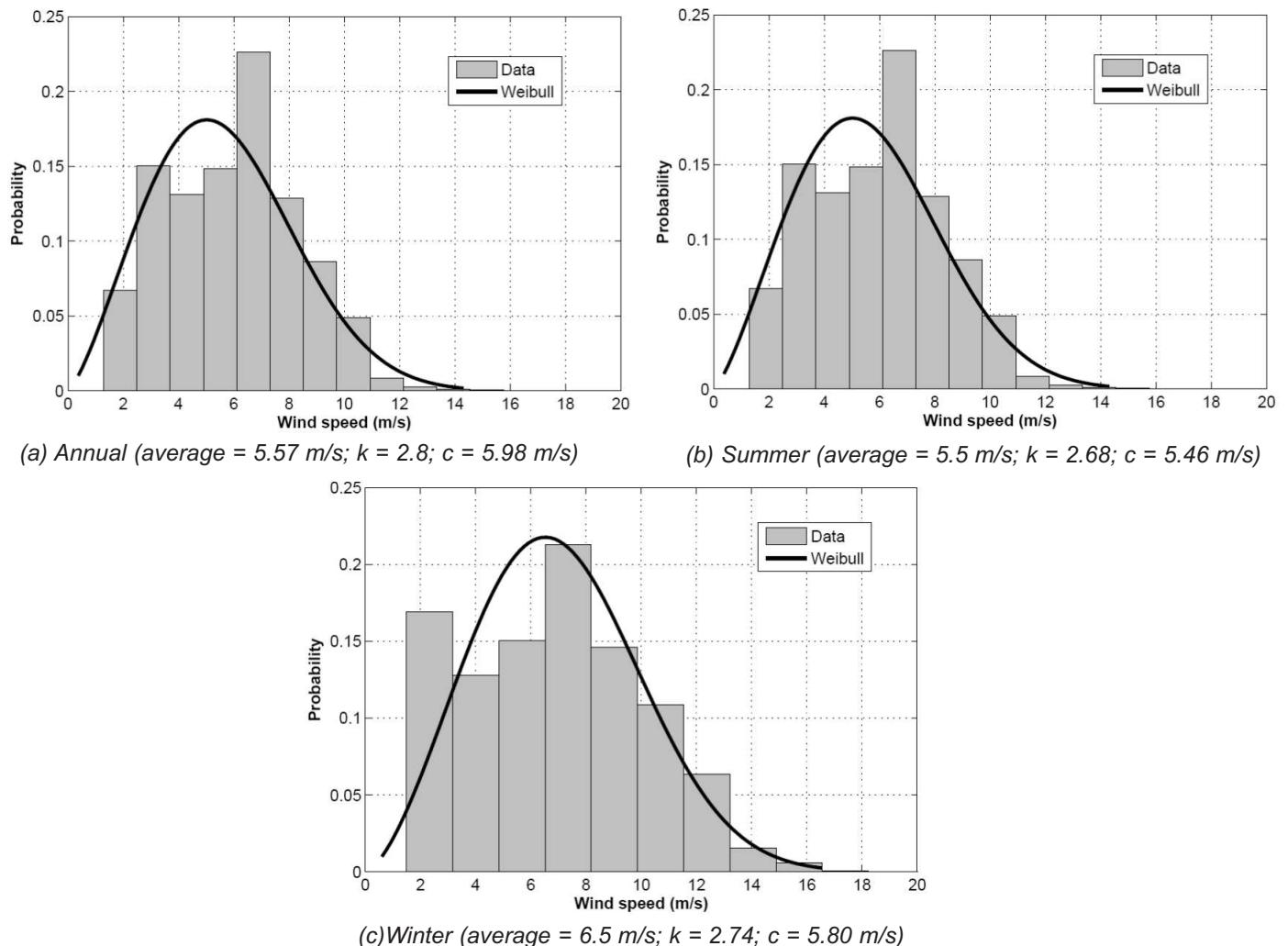


Figure 8: Annual and seasonal Weibull distribution curves fitted to ten years hourly wind speed data at Plaisance (60 m.a.g.l) from January 2005 to December 2014

Table 3 shows the Weibull scale c and shape parameters k of the data as well as the mean values \bar{v} as calculated from Equation (3) for different years during the period January 2005 to December 2014 at 60 m.a.g.l. For the annual data, the k parameter

varies from 2.24 to 2.68 and the scale parameter varies between 5.91 m/s to 7.08 m/s. For summer k varies between 2.02 and 2.80 and c varies between 5.68 m/s and 7.17 m/s while for winter the shape parameter ranges in the vicinity of 2.22 to 2.76 and

Table 3: Weibull parameters for annual, summer and winter wind data at Plaisance at 60 m altitude

Year	Annual			Summer			Winter		
	<i>k</i> (-)	(m/s)	\bar{v} (m/s)	<i>k</i> (-)	<i>c</i> (m/s)	\bar{v} (m/s)	<i>k</i> (-)	<i>c</i> (m/s)	\bar{v} (m/s)
2005	2.34	6.38	5.66	2.18	6.18	5.46	2.30	5.97	5.30
2006	2.68	6.84	6.08	2.80	7.17	6.40	2.64	6.50	5.77
2007	2.36	7.08	6.28	2.12	6.91	6.12	2.76	7.23	6.44
2008	2.46	6.81	6.03	2.46	6.67	5.91	2.47	6.95	6.16
2009	2.36	6.63	5.87	2.29	6.28	5.56	2.47	6.97	6.18
2010	2.51	6.54	5.79	2.56	6.02	5.33	2.57	7.02	6.23
2011	2.36	5.91	5.23	2.52	6.00	5.30	2.22	5.83	5.15
2012	2.62	6.87	6.10	2.54	6.56	5.82	2.74	7.16	6.37
2013	2.24	6.36	5.63	2.02	6.02	5.32	2.47	6.68	5.92
2014	2.25	6.18	5.46	2.27	5.68	5.02	2.30	6.66	5.89

the scale parameter from 5.83 m/s to 7.23 m/s. In general, the mean wind speed oscillates between 5 m/s to 6.5 m/s.

4.2 Wind farm

As stated previously, Plaisance benefits from a wind speed in the range of 5-7 m/s during winter season and 5-6 m/s during summer. According to 'The European Wind Energy Union' wind energy harvesting is classified as nearly good for $\bar{v} = 6.5$ m/s, good for $\bar{v} = 7.5$ m/s and very good for $\bar{v} \geq 8.5$ m/s (Garrad, 1991). Therefore, according to Table 2, the Mon Tresor Airport smart city at Plaisance is a suitable location for the installation of a wind farm since the mean wind speeds fall within category 1. The energy output during winter, as a function of mean wind speed for one wind turbine at hub height of 60 m at Plaisance, was estimated using Equation 6. The average annual energy output with one such turbine was observed to be around 280 MWh per annum at 60 m height. During summer for the same height (mean wind speed of 5.5 m/s), the total energy is expected to be around 150 MWh while for winter it is estimated to be 200 MWh (Figure 9).

5. Project cost

In this section, the economic viability of the proposed wind farm was analysed. The wind farm has a proposed capacity of 11 MW (40 turbines of capacity of 275 kW each). The cost of a wind turbine is mostly set by the manufacturer, and it is dependent on the rated power, e.g., a turbine rated more than 200 kW has an average cost of 1300 \$/kW (Gokcek & Genc, 2009; Gokcek *et al.*, 2007b; Matthew, 2006). In this case the cost of the Vergnet 275 kW was estimated to be around \$358 000. The proposed 11 MW wind farm has an initial installation cost of \$17.2 million, which includes the price of turbines and 20% for labour and other connections cost of the turbine, foundation, erection and so on (Ucar & Balo, 2009a). The operation, maintenance and repair costs were considered to be 25%

of the annual cost of the turbine (Palanichamy *et al.*, 2004). The economic optimization was performed by the Maximize Net Present Value (NPV) over $n=1$ to N and the Present Value Cost (PVC) as given by Equations 11 and 12.

$$NPV = -C_0 - C_1 n - C_2(n) - C_3 P_n + \sum_{t=1}^T (1+r)^{-t} E(n)(p_t + s_t - oc(n)) 10^{-6} \quad (11)$$

where C_0 is the fixed cost of site, C_1 is the cost of site infrastructure roads/internal cables etc, C_2 is the investment transformer connection, C_3 is the investment cost of turbines, the s_t is the subsidy level, the $oc(n)$ is the operational cost, the P_n is the installed capacity, the r is the interest rate and $E(n)$ is the energy yield.

$$PVC = I + C \left(\frac{1+i}{r-i} \right) \left(1 - \left(\frac{1+i}{1+r} \right)^t \right) - S \left(\frac{1+i}{1+r} \right)^t, \quad (12)$$

where PVC is the present value costs, the I is the initial total capital, the C_{omr} is the operation, maintenance and repair cost estimated at 25% of the annual cost of the turbines, the t is the 20 year lifetime, the i and r are the interest and inflation rate of Mauritius, which are 5% and 3.5% respectively and S is the scrap value which is taken to be 10% of the turbine price and civil work. These values are similar to those used by Ucar and Balo (2009b) and Bataineh and Dalalah (2013). In this case the PVC is approximately \$20 million and the NPV is \$32 million.

The energy obtained from a single Vergnet wind turbine is around 280 MWh per annum, which makes it around 11.2 GWh electricity produced by the wind farm per year. Therefore the unit cost of electricity is about 0.089 \$/kWh per year.

Assuming that the CEB is buying the energy produced at the current rate of 0.15 \$/kWh, then the profit per kWh is 0.061 \$/kWh. The yearly revenue generated by the wind farm is therefore estimated to be \$1.74 million. During its 20 years life-

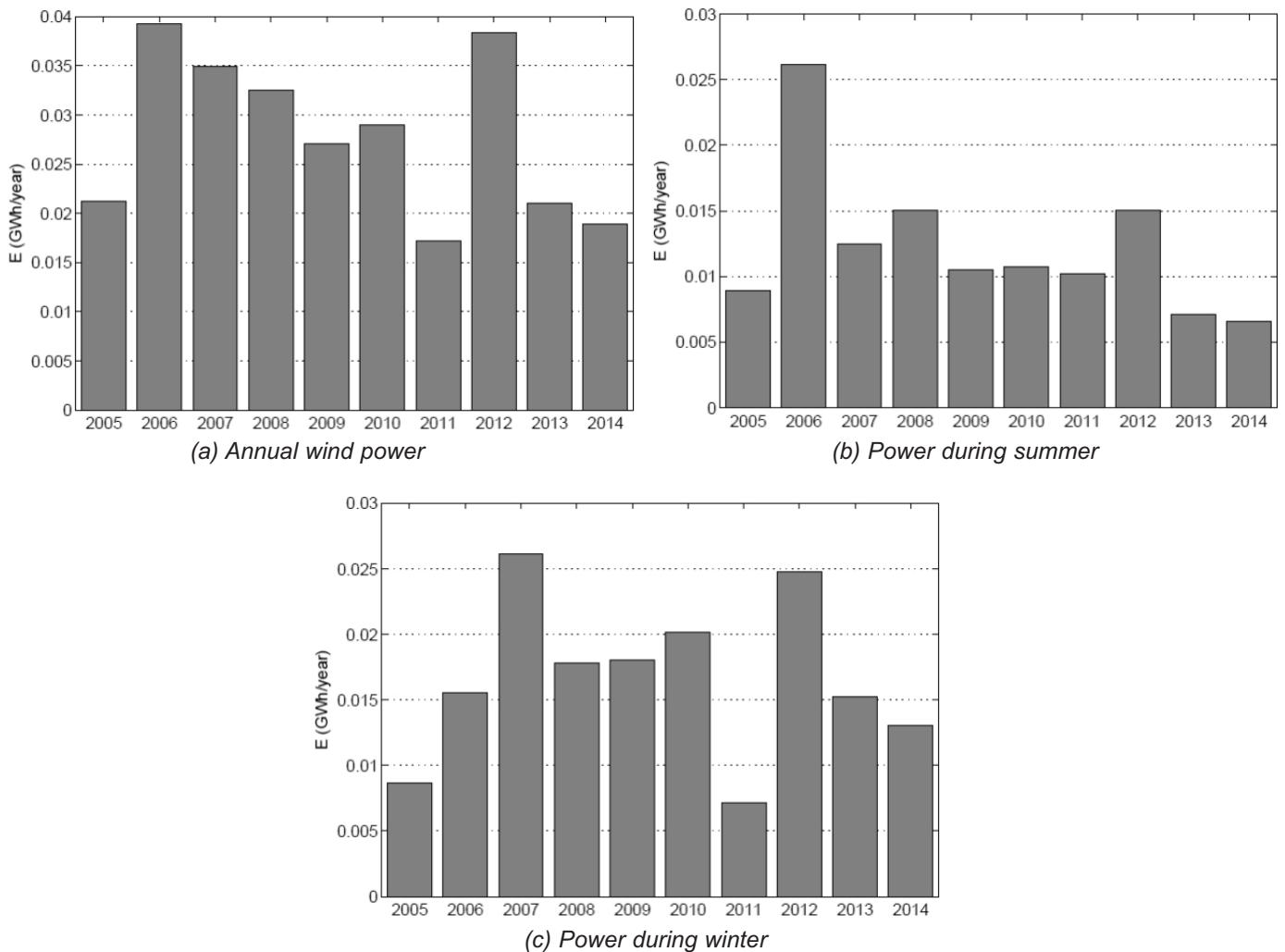


Figure 9: Energy output from the Vergnet GEV MP 275 kW wind turbine with hub height 60 m

time the revenue prediction is expected to have a 10% increase (CEB, 2014) in electricity purchase cost as given in Table 4. It is apparent that within eleven years, the initial investment would be recovered, emphasising that it is a profitable investment to have a wind farm at the proposed location.

Table 4: Yearly revenue excluding the yearly maintenance (in \$million)

Year	1-5	6-10	11-15	16-20
Profit each 5 year,	0.066	0.073	0.08	0.088
Revenue per year	1.74	2.1	2.3	
Total revenue (per 5 year)	8.7	9.5	10.5	11.6
Net revenue over the farm's lifetime, 20 years		40.3		

The internal rate of return (IRR) for this project, which is calculated from Equation 13 is 4.4% which makes this investment attractive (Deloitte 2014).

$$NPV = \sum (Period\ Cash\ Flow) / (1 + R)^T - Initial\ Investment \quad (13)$$

where the R is the interest rate and the T is the number of time periods which in this case is 20 years.

6. Conclusions

The main conclusions drawn from this investigation are as follows:

- The south-east coastal region of the island of Mauritius shows good wind energy potential.
- Part of the energy requirements for the Mon Tresor Airport Smart City can potentially be obtained from the wind throughout the year.
- The setting up of a wind farm in the south-east region of Mauritius is profitable with an estimated return on investment of around 11 years.

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